

Wetting and interfacial phenomena in relation to joining of advanced ceramics

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- **Introduction**

- Basics of wetting at high temperatures
- Basics of ceramic joining by brazing
- Methodologies: experimental complex for wetting studies

- **Examples of wetting and joining of SiC**

- dissolutive wetting: SiC/Ni-Si
- formation of new phases: SiC/Al-Ti
- active elements: SiC/Sn-Ti

- **Conclusions**

Wetting and joining

Metal/Ceramic or Ceramic/Ceramic **joining** is necessary in order to:

- integrate ceramic components into metallic structures;
- enhance the individual characteristics of different materials;
- assemble ceramics in complex shapes whenever sintering is difficult.

Within this field, many processes are possible, for example:

- Mechanical joining
- Adhesive bonding
- Diffusion bonding (solid state processes)
- Soldering ($<450^{\circ}\text{C}$)
- Brazing ($>450^{\circ}\text{C}$)
- Transient Liquid Phase Bonding



Liquid state processes

Wetting and joining

A **liquid based process** (e.g. brazing, transient liquid phase bonding) is often preferable:

- to limit surface preparation,
- to avoid high pressures
- when the adjoining surfaces are not flat.

When designing new joining methods to be realized through **liquid media**, it is fundamental to understand:

- ✓ how well the brazing alloy wets the adjoining surfaces;

→ **Wetting tests (sessile drop)**

- ✓ the chemical interactions between the liquid and the solid and how to control them;

→ **Microanalysis and calculation of multi-component phase diagrams**

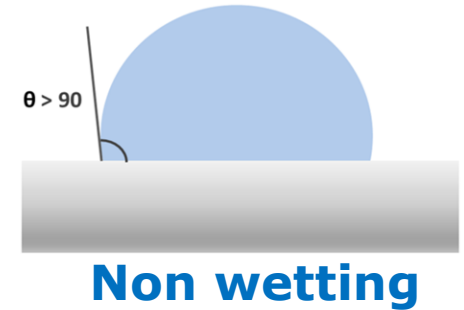
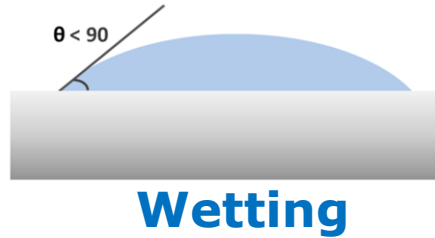
- ✓ the processing-microstructure-property relationship.

→ **Joints manufacturing and characterization (e.g. mechanical, corrosion, ageing tests)**

Wetting

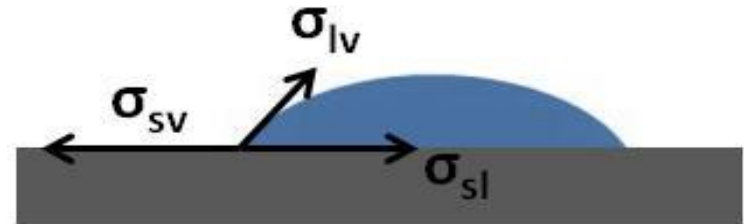
Wettability is the tendency of a liquid to contact a solid surface and it is measured in terms of the **contact angle** between the liquid and the solid.

Sessile drop



Young's equation: equilibrium contact angle in relation with the interfacial tensions between the three phases:

$$\sigma_{sv} = \sigma_{ls} + \sigma_{lv} \cos \theta$$



Young-Duprè equation: work of adhesion between the liquid and the solid:

$$W_{ad} = \sigma_{lv} (1 + \cos \theta)$$

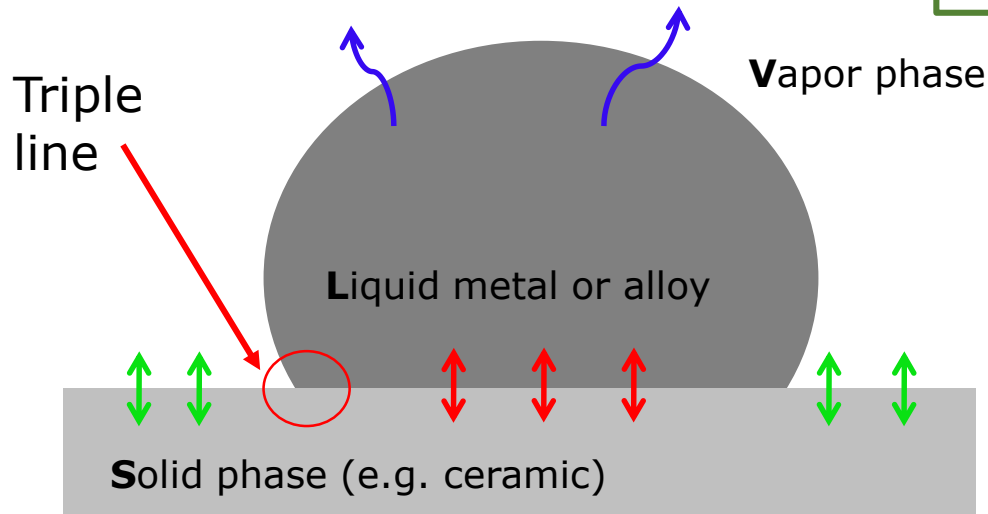
Gibbs adsorption (multicomponents):

$$d\sigma = -s dT - \sum_i \Gamma_i d\mu_i$$

Sessile drop

Sessile drop

σ_{LV} : surface tension of the liquid
 θ : contact angle



Young's equation

$$\cos \theta = (\sigma_{sv} - \sigma_{LS}) / \sigma_{LV}$$

• S/L interface

Dissolution of the solid phase, infiltration of the liquid into the solid, formation of interfacial compounds, adsorption of active elements (e.g. Ti, Cr)

• L/V interface

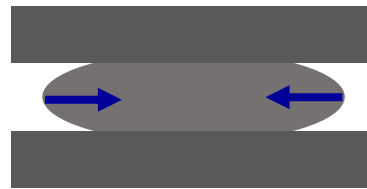
Evaporation, adsorption of gaseous compounds (e.g. oxygen), oxidation

• S/V interface

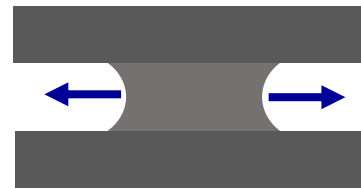
Oxidation-deoxidation of the surface, selective evaporation (e.g. SiO)

Wetting and joining

A braze alloy relies on capillarity to distribute the liquid alloy along the adjoining interfaces

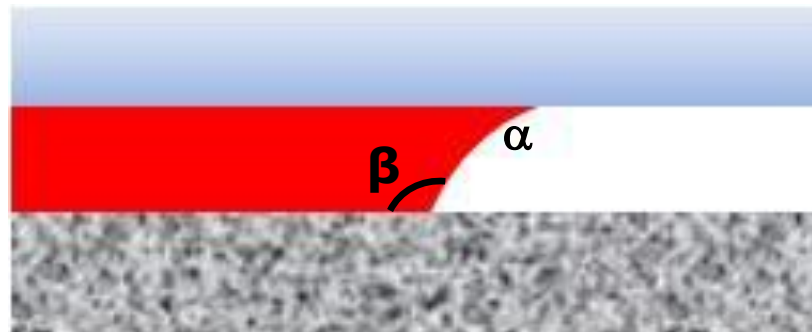
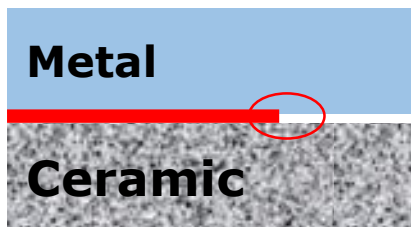


**Non-wetting
both substrates**



**Wetting both
substrates**

Conditions for spontaneous liquid infiltration



$$\alpha + \beta < 180^\circ$$

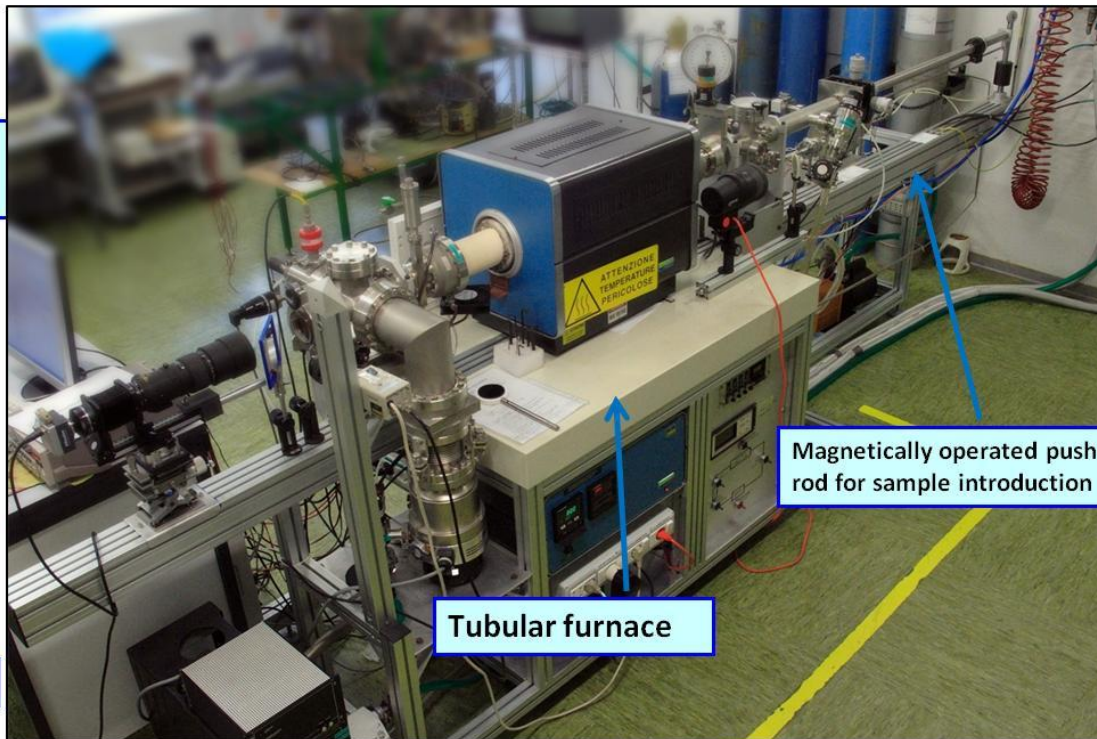
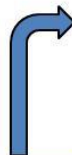
Experimental apparatus for sessile drop tests



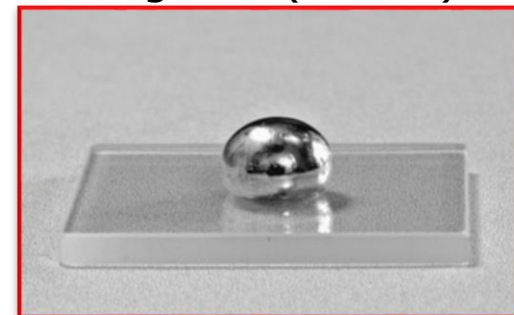
ASTRAView software



Digital Camera



Example of sessile drop during test ($\theta < 90^\circ$)



Example of sessile drop after cooling ($\theta > 90^\circ$)



$T_{\max} = 1600^\circ\text{C}$

Working atmosphere: Vacuum: 10^{-4} Pa @1500°C or gas mixtures (e.g. Ar, Ar/H₂, O₂, CO/CO₂) with analysis of PO₂ at inlet and outlet.

Fast heating and cooling: samples introduced into the experimental chamber through an external manipulator.

Analysis of wetting kinetics and surface tension by software (AstraView).

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• **Conclusions**

Nature of interfacial reactivity between SiC and liquid metals

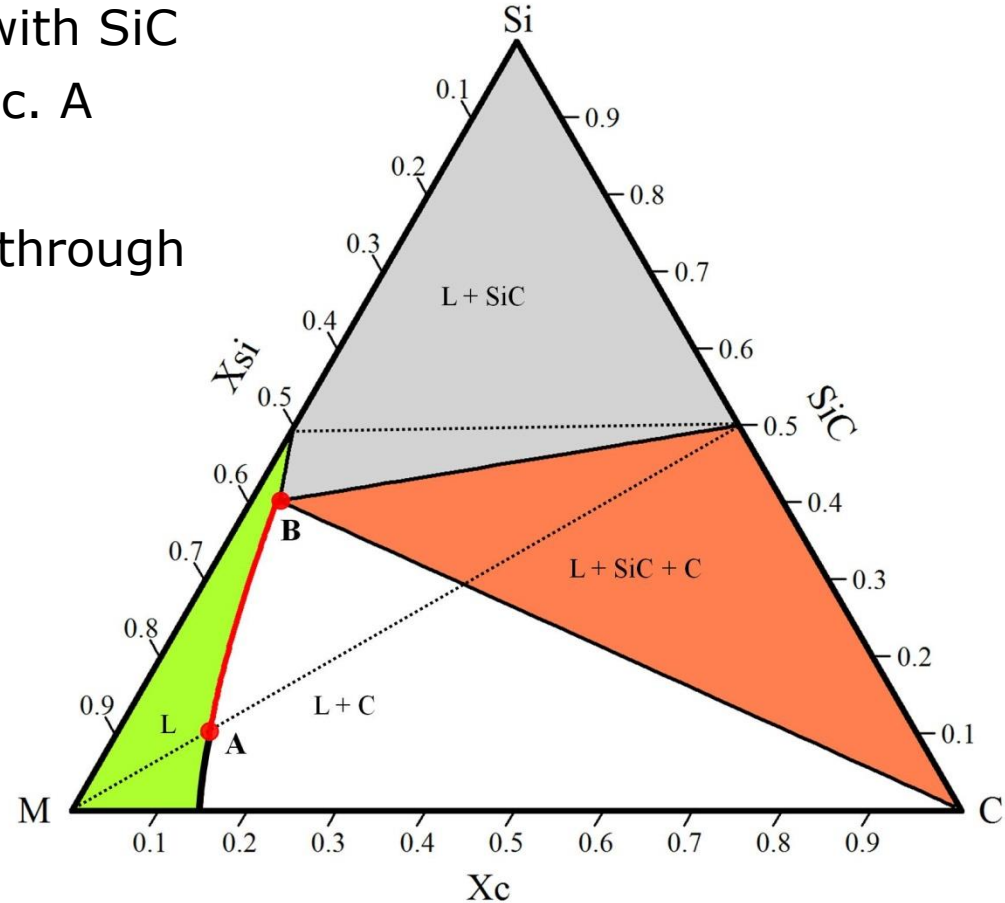
Reactivity for pure metals	Metal feature	Ex.
None		Pb, Au, Ag, Sn.
$\text{Me} + \text{SiC} \rightarrow \text{silicide} + \text{C}$	No stable carbide, stable silicides	Ni, Co, Fe, Cu
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The reactivity of liquid metals with SiC must be controlled in order to select the nature of the reaction products and the thickness of the reaction zone.

Dissolution in metal/SiC systems

Schematic isothermal section of M–Si–C phase diagram
(M = metal which does not form stable carbide)

- 1 - M (e.g. Co, Ni) in contact with SiC
- 2 - Dissolution of SiC until conc. A
- 3 - Precipitation of C
- 4 - Dissolution continues to B through the red line

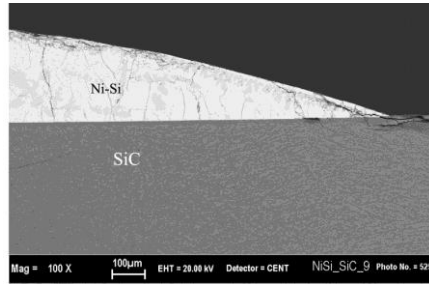


Dissolution in metal/SiC systems

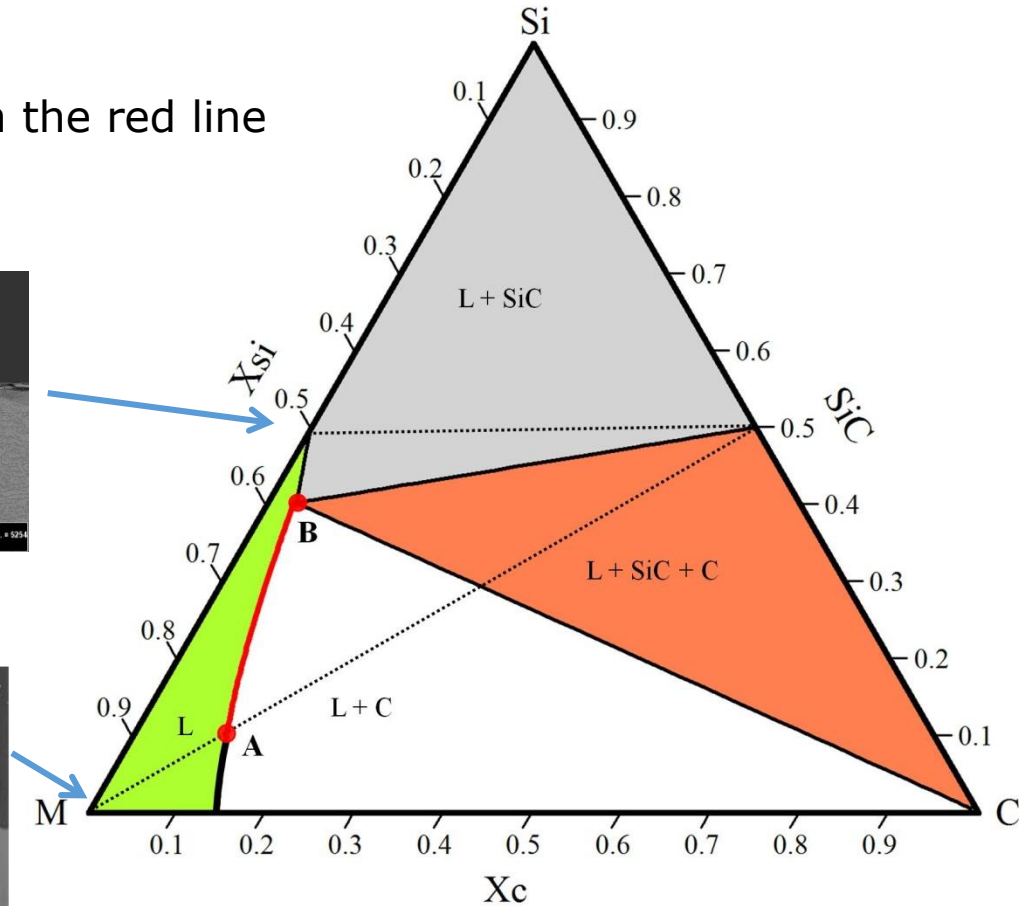
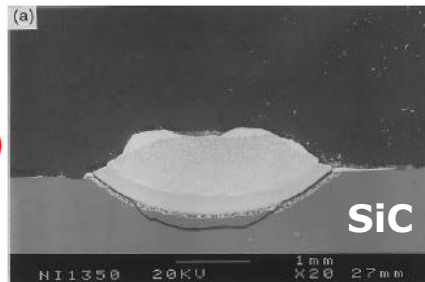
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Schematic isothermal section of M-Si-C phase diagram
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Ni-Si alloy:**
NON reactive



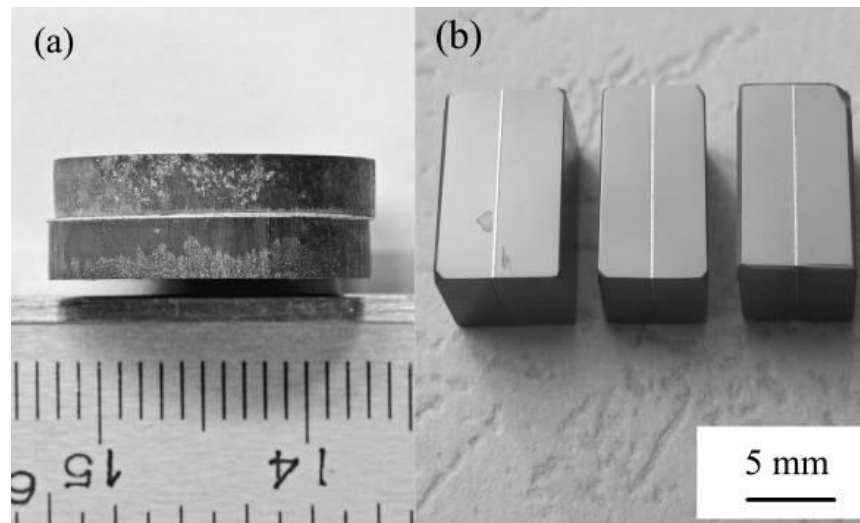
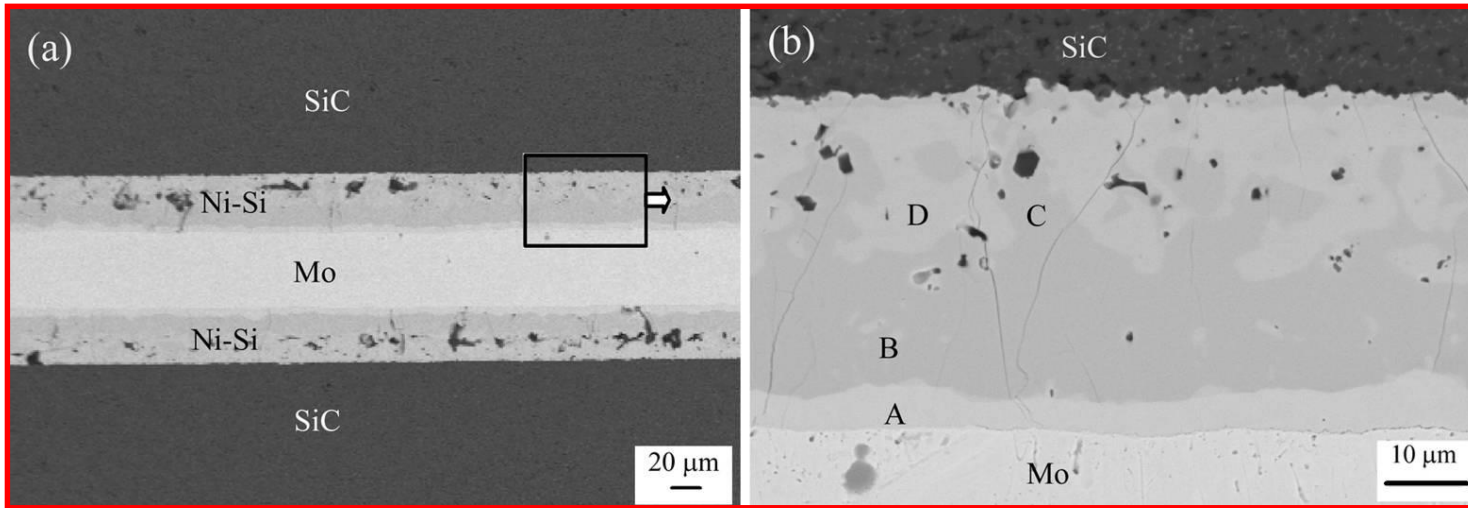
Pure Ni*:
reactive (dissolutive)



* Rado C., Kalogeropoulos S., Eustathopoulos N., Acta Materialia **47** (1999) 461-473

Liu G.W., Valenza F., Muolo M.L., Qiao G.J., Passerone A., J. of Materials Science **44 (2009) 5990-5997

SiC-SiC joining with Mo interlayer, 1350°C – 10 min



Liu G.W., Valenza F., Muolo M.L., Passerone A., SiC/SiC and SiC/Kovar joining by Ni-Si and Mo interlayers, J Mater Sci 45(16) (2010) 4299-4307

Nature of interfacial reactivity between SiC and liquid metals

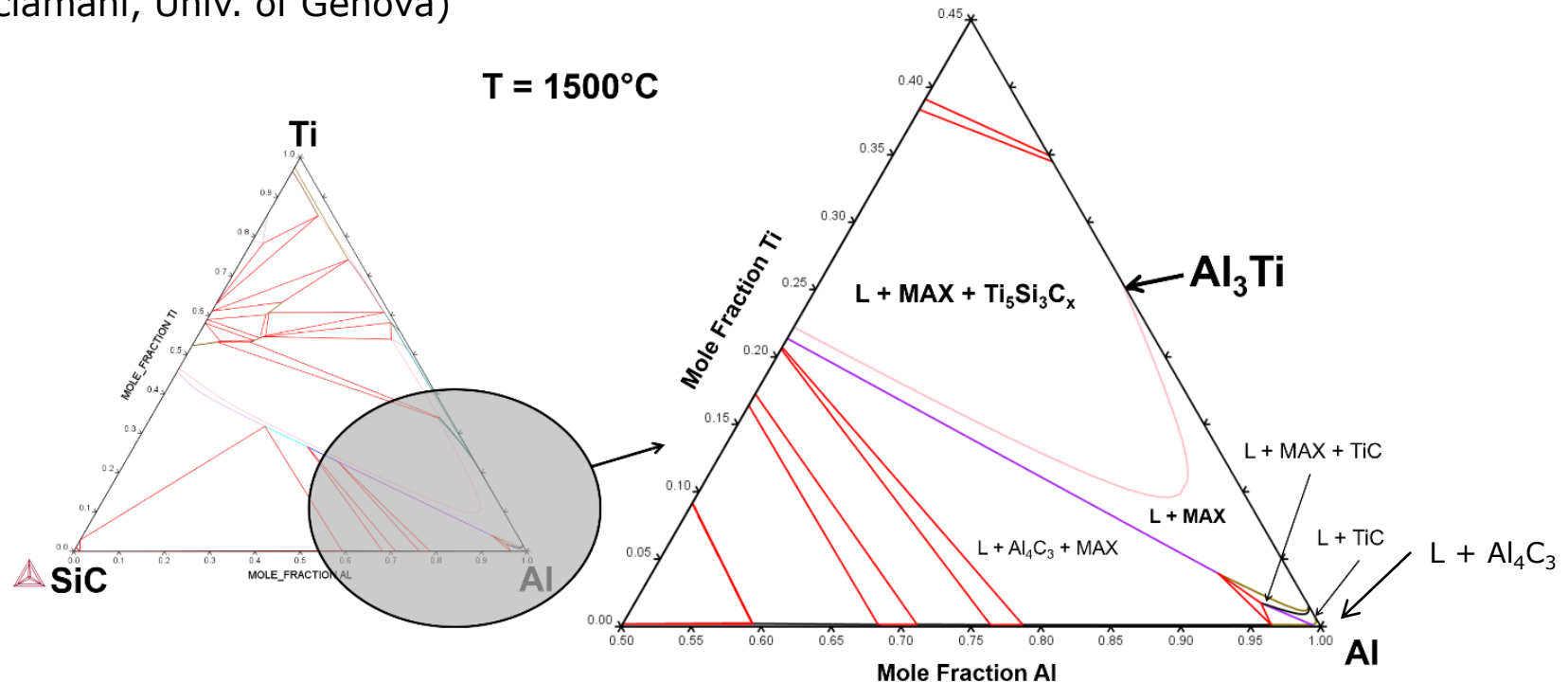
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Wetting of SiC by Al + Ti

SiC-Al-Ti system

SiC-Al-Ti isothermal section – Al-rich corner

(determination of multicomponent phase diagram by CALPHAD, collaboration with prof. Cacciamani, Univ. of Genova)

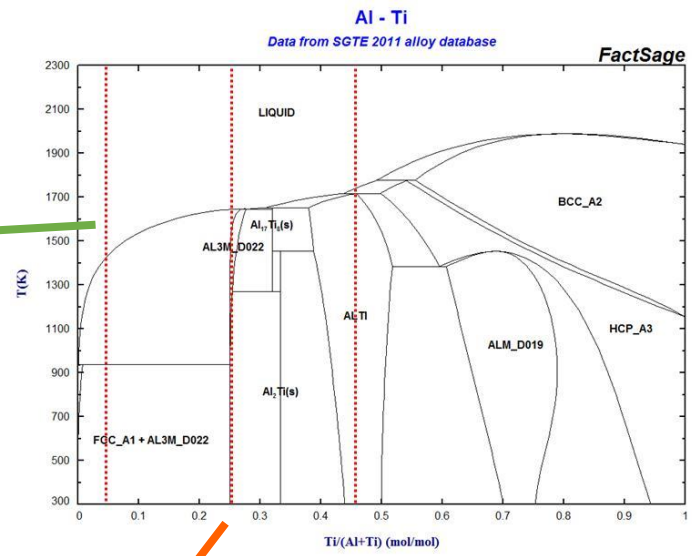
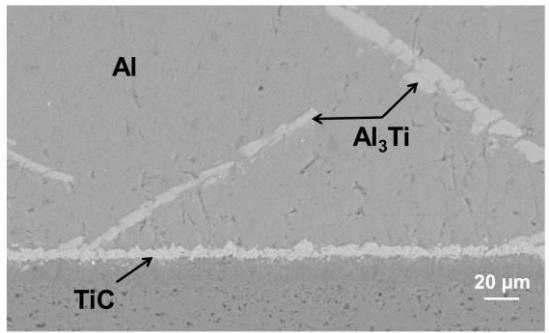
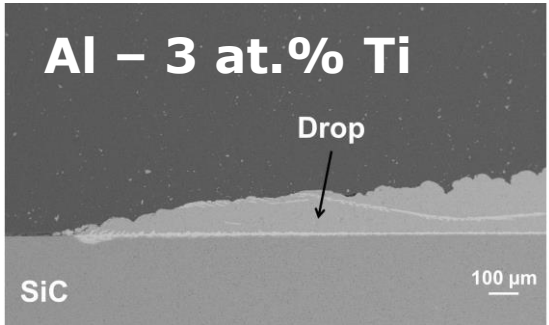


Main goal: to obtain SiC/SiC joints through the **in-situ formation of a $Ti_3Si(Al)C_2$ phase** starting from simple Al-Ti interlayers. Similarly to a **transient liquid phase bonding process**, the in-situ formation of the desired phase at the process temperature would allow to overcome the thermal stresses associated with the solidification by cooling of the interfacial phases over a broad temperature range.

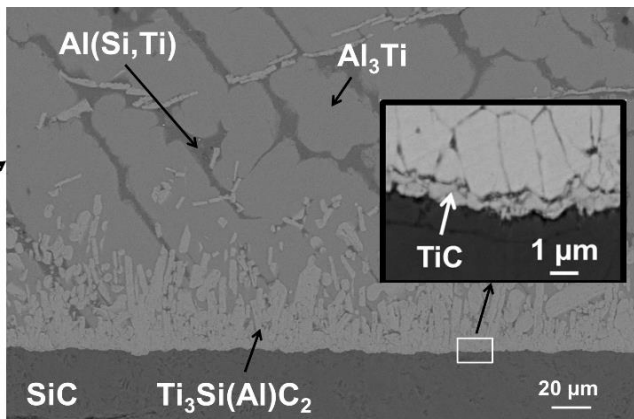
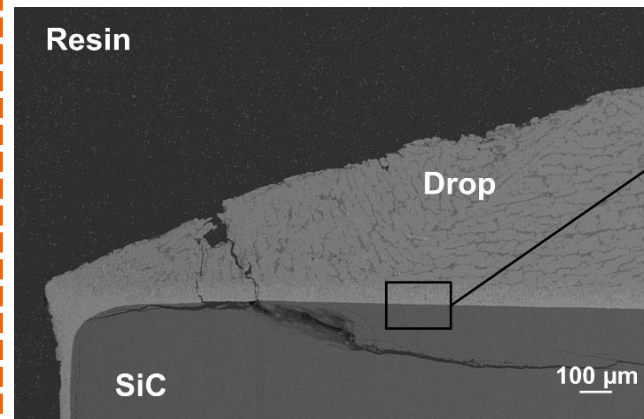
S.Gambaro, F.Valenza, G.Cacciamani, M.L. Muolo, A.Passerone, F.Toche, R.Chiriach, O.Dezellus, High-Temperature-Reactivity evaluation of Al-Ti alloys in contact with SiC, submitted to Journal of Materials Science

Wetting results: microstructures

T = 1500°C



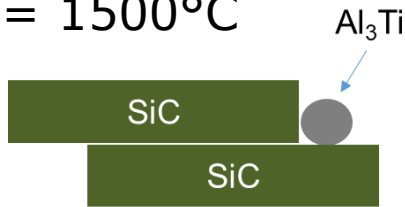
Al – 25 at.% Ti (Al₃Ti)



Valenza, F., Gambaro, S., Muolo, M.L., Salvo, M., Casalegno, V., *Wetting of SiC by Al-Ti alloys and joining by in-situ formation of interfacial Ti₃Si(Al)C₂*, Journal of the European Ceramic Society, 38 (2018) 3727-3734

Joining of SiC by in-situ formation of $Ti_3Si(Al)C_2$ phase

$T = 1500^\circ C$

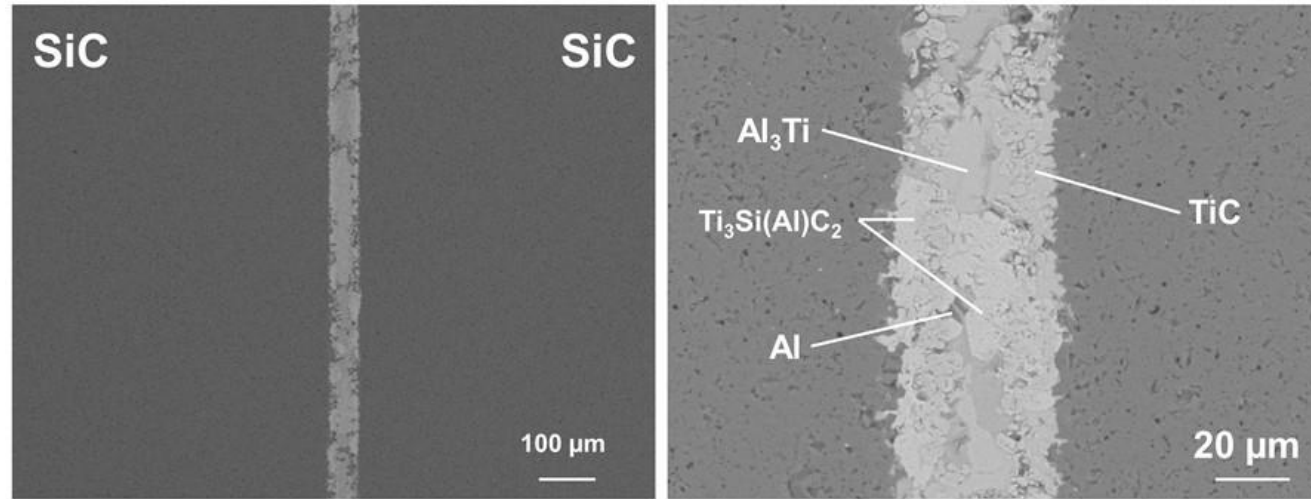


Infiltration of Al_3Ti

No cracks

Resulting phases:

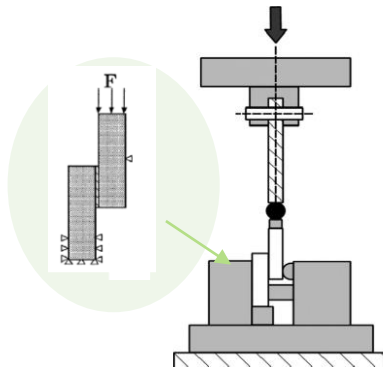
$Ti_3Si(Al)C_2$, Al_3Ti , Al



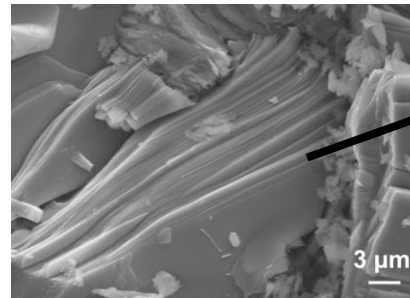
Mechanical tests

at Politecnico di Torino

$\tau = 296 \text{ MPa} \pm 20$

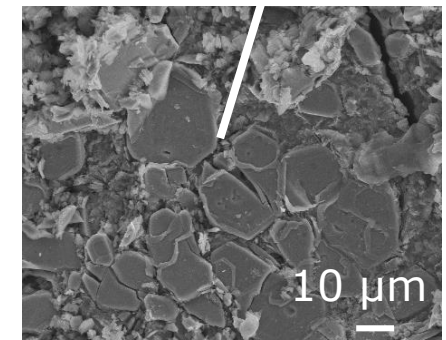
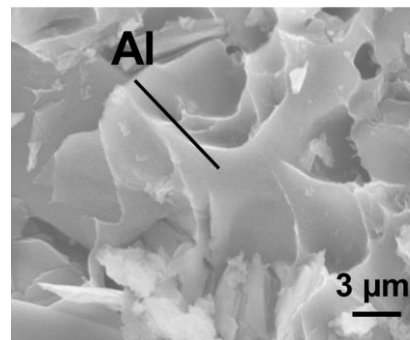


Fracture surfaces



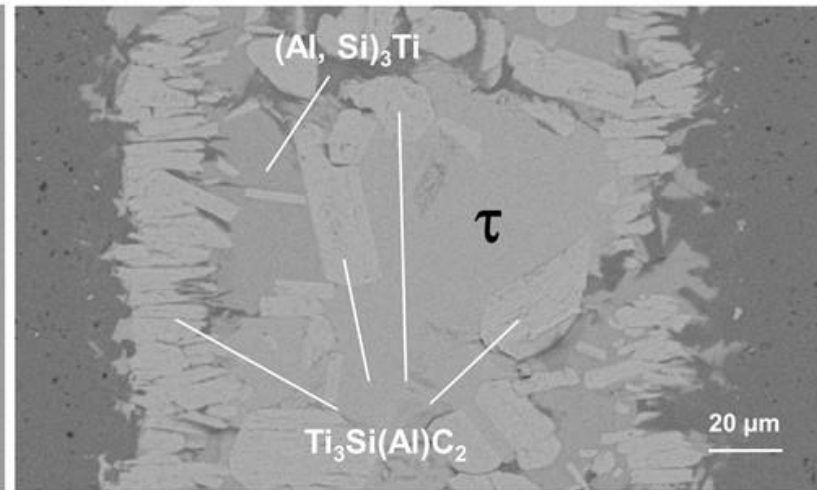
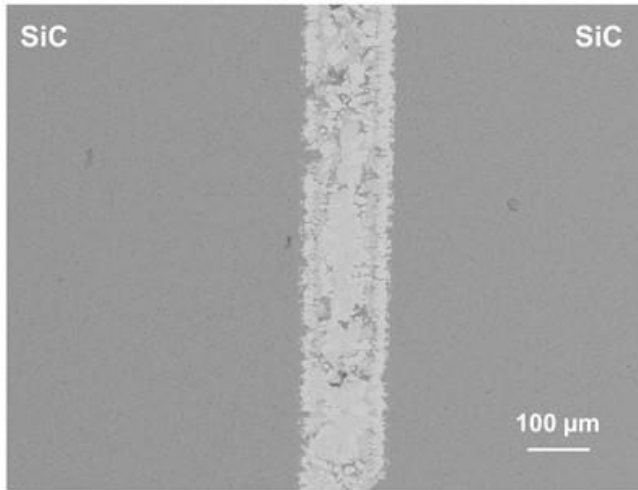
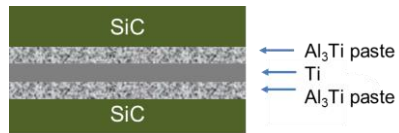
Kink bands in $Ti_3Si(Al)C_2$

Transgranular fracture in TiC



Joining of SiC by in-situ formation of $Ti_3Si(Al)C_2$ phase

Al_3Ti / Ti foil / Al_3Ti



No cracks

Thickness: $\sim 50 \mu m$

Resulting phases: $Ti_3Si(Al)C_2$, $(Al, Si)_3Ti$, τ phase in the Al-Si-Ti phase diagram (Al 13, Si 34, Ti 53 at.%)

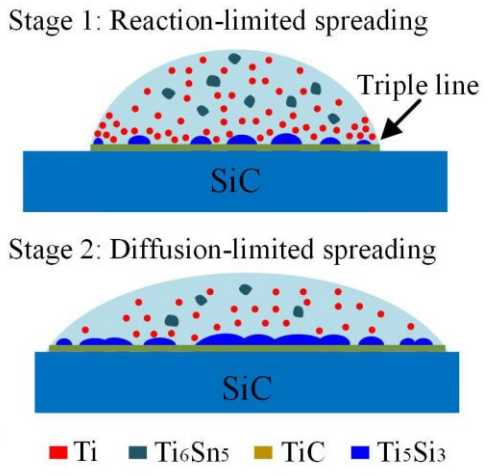
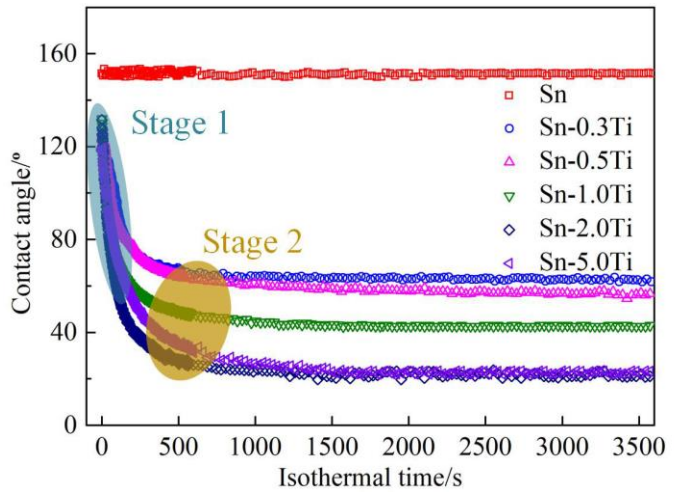
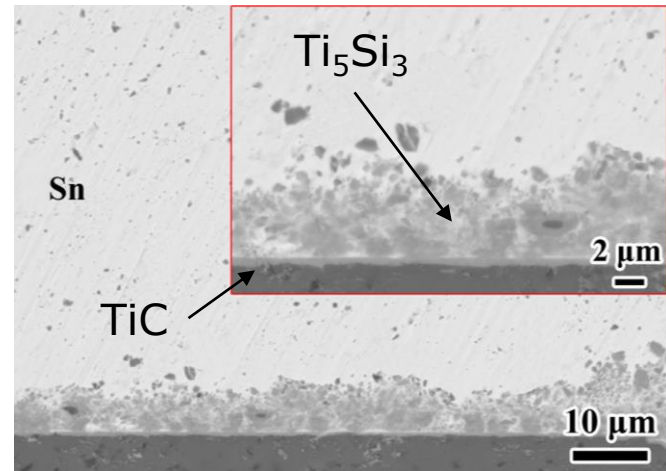
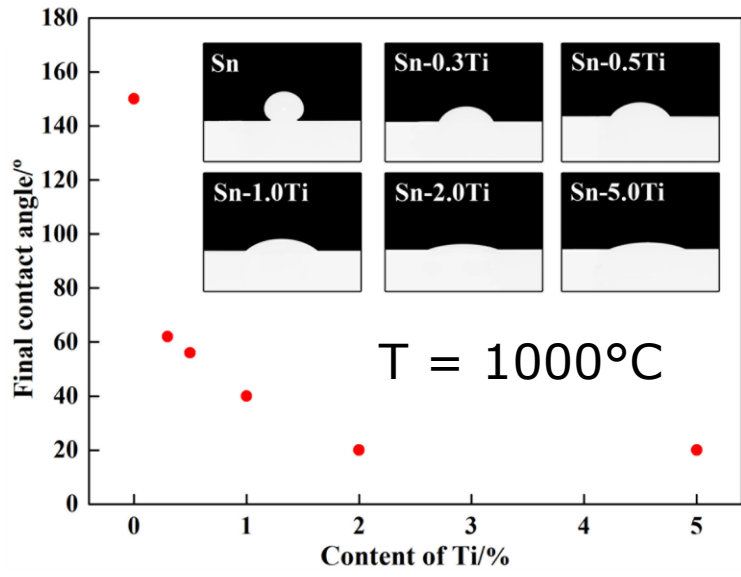
$$\tau = 85 \text{ MPa}$$

Nature of interfacial reactivity between SiC and liquid metals

Reactivity for pure metals	Metal feature	Ex.
None		Pb, Au, Ag, Sn
$\text{Me} + \text{SiC} \rightarrow \text{silicide} + \text{C}$	No stable carbide, stable silicides	Ni, Co, Fe, Cu
$\text{Me} + \text{SiC} \rightarrow \text{Si} + \text{carbide}$	Stable carbides	V, Al, Nb
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Wetting of Sn-Ti alloys on SiC

Wetting of Sn-Ti alloys on SiC



Song X, Passerone A, Fu W, Hu S, Niu C, Zhao Y, Wang M, Valenza F, Wetting and spreading behavior of Sn-Ti alloys on SiC, *Materialia* 3 (2018), 57-63

Conclusions

The study of **metal-ceramic interfaces at high temperature** is relevant in applications which involve the combination of these two class of materials (e.g. production of metal-ceramic joints, casting of special alloys etc.).

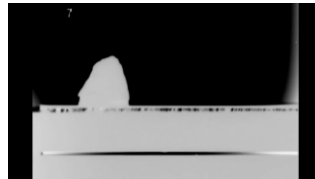
Joining processes for ceramics based on liquid phases (e.g. brazing) need the knowledge of liquid-solid interfacial phenomena.

In particular, it is fundamental to investigate:

- the wettability of liquid alloys on ceramics
- the evolution of interfaces
- the interfacial reactions and how to control them

Phase diagrams could assist the choice of the most proper braze compositions in order to promote wetting, to avoid deleterious reactions (e.g. dissolution) or to get new phases.

Active metals could be used to enhance the wetting behaviour of non-wetting alloys.



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Prof. M. Ferraris, Prof. V. Casalegno, Prof. M. Salvo (Politecnico di Torino):
mechanical testing

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Thank you

for your attention!